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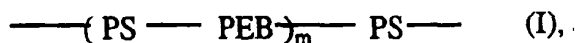
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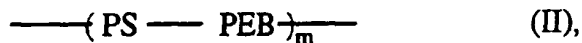
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(54) **Thermoplastic resin composition**

(57) A thermoplastic resin composition comprising a propylene polymer component, a styrene-containing elastomer component and talc. The propylene polymer component may be an ethylene-propylene block copolymer, polypropylene resin, a mixture of at least two propylene polymers each having different melt flow rate. The styrene-containing elastomer may be an elastomeric styrene-containing block copolymer represented by the following formula (I) or (II):



and



wherein PS is a polystyrene block, PEB is a poly(ethylene-butene) block and m is an integer of 1 or more. Also, the styrene-containing elastomer may be a mixture of the elastomeric styrene-containing block copolymers having different melt flow rates.

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Description

BACKGROUND OF THE INVENTION

5 The present invention relates to a thermoplastic resin composition comprising a propylene polymer, an elastomeric styrene-containing block copolymer and a talc. The resin composition is excellent, in particular, in injection moldability and provides molded articles having a good mechanical strength.

Polypropylene has a good mechanical strength and a good moldability in spite of its low density, and is widely utilized in various application fields. However, polypropylene is insufficient in the impact resistance and the heat resistance. To improve these defects, various polypropylene resin compositions, for example, those comprising an ethylene-propylene block copolymer produced by a multi-stage polymerization, a rubber component such as an ethylene-propylene copolymer rubber and an ethylene-butene copolymer rubber, and an inorganic filler such as talc have been proposed.

Japanese Patent Laid-Open No. 1-149845 discloses a resin composition comprising (a) 59 to 74 weight % a propylene-ethylene block copolymer, (b) 35 to 20 weight % of an ethylene-propylene copolymer rubber, and (c) 3 to 6 weight % of talc having a specific surface area of 30,000 cm²/g or more and an average particle size of 0.5 to 2.0 μ m. The propylene-ethylene block copolymer has an ethylene content of 1 to 7 weight % and a melt flow rate of 15 to 50 g/10 min. The propylene-ethylene block copolymer is further specified by containing 5 to 12 weight % of a boiling xylene solubles having an ethylene content of 20 to 60 weight %. The ethylene-propylene copolymer rubber is characterized by a propylene content of 20 to 60 weight % and a Mooney viscosity (ML₁₊₄(100°C)) of 100 to 150. The resin composition contains a fine talc. The fine particles of talc are easily agglomerated together to deteriorate a balance of mechanical strength such as hardness, stiffness, impact strength at low temperature, etc. Also, a great specific surface area of the fine talc makes the fine talc particles highly adherent, and the additives are adhered on the fine particles of talc to fail in exhibiting their ability. To eliminate this problem, it has been proposed to subject the fine talc to a surface treatment by a surface-treating agent of aminosilane type, titanate type, etc. to improve the dispersibility of talc thereby preventing the additives from being adhered to the talc. However, such a proposal is still insufficient.

To improve the impact resistance of the conventional polypropylene, it has been also proposed to increase the content of the ethylene-propylene copolymer block in the ethylene-propylene block copolymer, or to add a rubber component such as an ethylene-propylene copolymer rubber and an ethylene-butene copolymer rubber in an increased amount. However, these modification is not successful because the fluidity of the resultant resin composition is decreased. Also, the addition of the rubber component in a large amount reduces the heat resistance and the surface hardness of the molded articles.

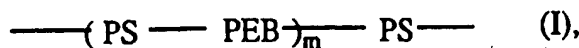
In view of improving the productivity, the demand for making the molded articles large in their size and reducing the thickness of the molded articles. This demand in turn requires to provide a molding material of high performance. To meet such a demand, it is inevitable for the molding material to be further improved in its fluidity and be made more sufficient in its performance. However, the conventional molding material comprising an ethylene-propylene block copolymer and a polyolefin elastomer has failed to meet this demand because the demand exceeds the limit of improvement achieved by the conventional molding material.

OBJECT AND SUMMARY OF THE INVENTION

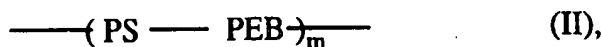
Accordingly, an object of the present invention is to provide a thermoplastic resin composition having a good moldability and providing a molded article of a good mechanical strength.

As a result of the intense research in view of the above object, the inventors have found that the above problems in the prior art can be eliminated by blending a specific ethylene-propylene block copolymer or a specific propylene resin with a specific elastomeric styrene-containing block copolymer and talc. The inventors have further found that the above problems in the prior art can also be eliminated by blending a least two different kinds of propylene polymers having different melt flow rates with a specific elastomeric styrene-containing block copolymer and talc. The present invention has been accomplished based on the above findings.

Thus, in a first aspect of the present invention, there is provided a thermoplastic resin composition comprising: (A) 30 to 80 weight % of an ethylene-propylene block copolymer having a melt flow rate of 30 to 200 g/10 min and comprising (a) 70 to 99 weight % of a crystalline propylene polymer block and (b) 1 to 30 weight % of an ethylene-propylene copolymer block having an ethylene content of 20 to 80 weight % and an intrinsic viscosity $[\eta]_{\text{CXS}}$ of 2 to 7 dl/g; (B) 10 to 30 weight % of an elastomeric styrene-containing block copolymer having a melt flow rate of 0.5 to 40 g/10 min and a polystyrene block content of 10 to 30 weight %, and being represented by the following formula (I) or (II):



5 and

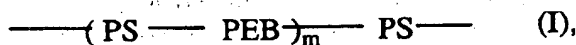


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wherein PS is the polystyrene block, PEB is an poly(ethylene-butene) block and m is an integer of 1 or more; and (C) 10 to 40 weight % of talc having an average particle size of 5 μm or less.

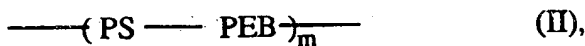
In a second aspect of the present invention, there is provided a thermoplastic resin composition comprising: (A) 30 to 80 weight % of a polypropylene resin having a melt flow rate of 20 to 200 g/10 min, an isotactic pentad fraction of 95 % or more and a copolymer block content of 0 to 2 weight %; (B) 10 to 30 weight % of an elastomeric styrene-containing block copolymer having a melt flow rate of 0.5 to 40 g/10 min and a polystyrene block content of 10 to 30 weight %, and being represented by the following formula (I) or (II):

20



and

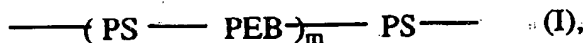
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30 wherein PS is the polystyrene block, PEB is an poly(ethylene-butene) block and m is an integer of 1 or more; and (C) 10 to 40 weight % of talc having an average particle size of 5 μm or less.

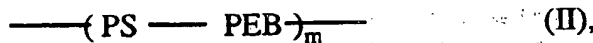
In a third aspect of the present invention, there is provided a thermoplastic resin composition comprising: (A) 30 to 80 weight % of an ethylene-propylene block copolymer having a melt flow rate of 30 to 200 g/10 min and comprising (a) 70 to 99 weight % of a crystalline propylene polymer block and (b) 1 to 30 weight % of an ethylene-propylene copolymer block having an ethylene content of 20 to 80 weight % and an intrinsic viscosity $[\eta]_{\text{CXS}}$ of 2 to 7 dl/g; (B) 5 to 30 weight % of a binary elastomer comprising (a) 40 to 80 weight % of at least one elastomeric styrene-containing block copolymer having a melt flow rate of 0.5 to 3 g/10 min and a polystyrene block content of 10 to 30 weight % and (b) 20 to 60 weight % of another at least one elastomeric styrene-containing block copolymer having a melt flow rate of 4 to 100 g/10 min and a polystyrene block content of 10 to 30 weight %, and each of the elastomeric styrene-containing block copolymers constituting the binary elastomer being represented by the following formula (I) or (II):

40



45

and

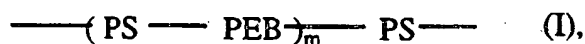


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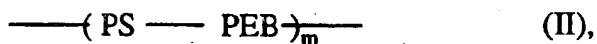
wherein PS is the polystyrene block, PEB is an poly(ethylene-butene) block and m is an integer of 1 or more; and (C) 10 to 40 weight % of talc having an average particle size of 5 μm or less.

In a fourth aspect of the present invention, there is provided a thermoplastic resin composition comprising: (A) 30 to 80 weight % of a polypropylene resin having a melt flow rate of 20 to 200 g/10 min, an isotactic pentad fraction of 95 % or more and a copolymer block content of 0 to 2 weight %; (B) 5 to 30 weight % of a binary elastomer comprising (a) 40 to 80 weight % of at least one elastomeric styrene-containing block copolymer having a melt flow rate of 0.5 to 3 g/10 min and a polystyrene block content of 10 to 30 weight % and (b) 20 to 60 weight % of another at least one

elastomeric styrene-containing block copolymer having a melt flow rate of 4 to 100 g/10 min and a polystyrene block content of 10 to 30 weight %, and each of the styrene-containing block copolymers constituting the binary elastomer being represented by the following formula (I) or (II):

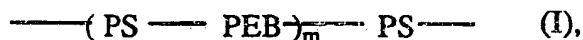


and

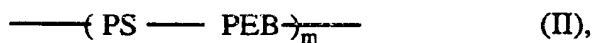


wherein PS is the polystyrene block, PEB is a poly(ethylene-butene) block and m is an integer of 1 or more; and (C) 10 to 40 weight % of talc having an average particle size of 5 μm or less.

In a fifth aspect of the present invention, there is provided a thermoplastic resin composition comprising: (A) 10 to 50 weight % of at least one first propylene polymer component selected from the group consisting of a first homopolypropylene and a first ethylene-propylene block copolymer, each having a melt flow rate of 2 to 30 g/10 min; (B) 10 to 50 weight % of at least one second propylene polymer component selected from the group consisting of a second homopolypropylene and a second ethylene-propylene block copolymer, each having a melt flow rate of 50 to 1000 g/10 min; (C) 10 to 30 weight % of an elastomeric styrene-containing block copolymer having a melt flow rate of 0.5 to 40 g/10 min and a polystyrene block content of 10 to 30 weight %, and being represented by the following formula (I) or (II):



and

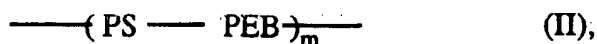


wherein PS is the polystyrene block, PEB is a poly(ethylene-butene) block and m is an integer of 1 or more; and (D) 10 to 40 weight % of talc having an average particle size of 5 μm or less.

In a sixth aspect of the present invention, there is provided a thermoplastic resin composition comprising: (A) 10 to 50 weight % of at least one first propylene polymer component selected from the group consisting of a first homopolypropylene and an ethylene-propylene random copolymer, the first homopolypropylene having a melt flow rate of 2 to 30 g/10 min and an isotactic pentad fraction of 90 to 95%, and the ethylene-propylene random copolymer having a melt flow rate of 2 to 30 g/10 min and an ethylene content of 0.1 to 1 weight %; (B) 10 to 50 weight % of a second homopolypropylene having a melt flow rate of 50 to 1000 g/10 min; (C) 10 to 30 weight % of an elastomeric styrene-containing block copolymer having a melt flow rate of 0.5 to 40 g/10 min and a polystyrene block content of 10 to 30 weight %, and being represented by the following formula (I) or (II):



and



wherein PS is the polystyrene block, PEB is a poly(ethylene-butene) block and m is an integer of 1 or more; and (D) 10 to 40 weight % of talc having an average particle size of 5 μm or less.

DETAILED DESCRIPTION OF THE INVENTION

[1] FIRST THERMOPLASTIC RESIN COMPOSITION

5 The first preferred thermoplastic resin composition of the present invention contains the following (A) a propylene polymer component, (B) a styrene-containing elastomer component, and (C) talc as the essential components.

A Propylene polymer component

10 The first preferred thermoplastic resin composition contains an ethylene-propylene block copolymer or a propylene resin as the propylene polymer component in an amount of 30 to 80 weight %, preferably 50 to 80 weight % based on the total weight of the components (A), (B) and (C). If the content is less than 30 weight %, the stiffness, heat resistance and hardness of the molded articles are poor, and mechanical strength and ductility are reduced when exceeding 80 weight %.

A-1 Ethylene-propylene block copolymer

15 The ethylene-propylene block copolymer used in the present invention substantially comprises (a) a crystalline propylene polymer block composed of repeating propylene units and (b) an ethylene-propylene copolymer block composed of randomly copolymerized ethylene units and propylene units, and optionally contains (c) a crystalline ethylene polymer block composed of repeating ethylene units. The content of the crystalline propylene polymer block (a) is 70 to 99 weight %, preferably 85 to 97 weight %, and the content of the ethylene-propylene copolymer block (b) is 1 to 30 weight %, preferably 3 to 15 weight %, each based on the total weight of (a) and (b). If the each content is outside the above range, the mechanical properties of the resulting molded articles are not well balanced. The crystalline ethylene polymer block (c) may be optionally or unintentionally contained in an amount of 5 weight % or less based on the weight of the ethylene-propylene block copolymer.

The crystalline propylene polymer block is derived from a propylene homopolymer or a propylene copolymer containing a small amount (5 mol % or less) of α -olefin such as butene-1, octene-1, etc. as a comonomer component.

20 The ethylene-propylene copolymer block is an ethylene-propylene copolymer of a low crystallinity. The ethylene content in the ethylene-propylene copolymer block is 20 to 80 weight %, preferably 35 to 65 weight % based on the total weight of the ethylene-propylene copolymer block. If the ethylene content is outside the above range, the ductility of the resin composition is insufficient. The ethylene-propylene copolymer block may contain α -olefin such as butene-1, octene-1, etc. as the third component in an amount 5 mol % or less. An intrinsic viscosity ($[\eta]_{\text{CXS}}$) is 2 to 7 dl/g, preferably 3 to 5 dl/g. When $[\eta]_{\text{CXS}}$ is less than 2 dl/g, flow marks occur on the surface of the molded articles. On the other hand, the resin composition is less flowable when exceeding 7 dl/g.

25 The crystalline ethylene polymer block is optional and unintentionally incorporated into the ethylene-propylene block copolymer during the formation of the ethylene-propylene copolymer block in a slight amount, and may contain the same comonomer component as the third component of the ethylene-propylene copolymer block in an amount of 5 mol % or less.

30 The ethylene-propylene block copolymer comprising the above blocks has a melt flow rate (MFR) of 30 to 200 g/10 min, preferably 30 to 120 g/10 min when measured at 230°C under a load of 2.16 kgf. When the MFR is less than 20 g/10 min, the resin composition is less flowable and the moldability, in particular, the injection moldability is deteriorated. An MFR exceeding 200 g/10 min undesirably reduces the mechanical strength of the molded articles.

35 In place of the ethylene-propylene copolymer block described above, an olefin elastomer such as an ethylene-propylene copolymer rubber and an ethylene-butene copolymer rubber may be used as far as the olefin elastomer has the ethylene content and $[\eta]_{\text{CXS}}$ in the above range. In this case, the MFR of the resin composition is preferred to be regulated within the range of 30 to 200 g/10 min by adding a crystalline propylene homopolymer.

40 The ethylene-propylene block copolymer may be produced by a known method. For example, it may be produced by a multistage polymerization comprising (a) forming the crystalline propylene polymer block by polymerizing propylene monomer with or without a slight amount of a comonomer by a single stage or multistage as employed in a known propylene polymerization; and (b) successively forming the ethylene-propylene copolymer block by copolymerizing ethylene monomer and propylene monomer in a single stage or multistage.

45 In the present invention, the amount of each of the crystalline propylene polymer block, the ethylene-propylene copolymer block and the crystalline ethylene polymer block was determined as follows. An amount of the ethylene-propylene block copolymer was introduced into a boiling xylene to dissolve only the ethylene-propylene copolymer block. The insoluble residue containing the crystalline propylene polymer block and the crystalline ethylene polymer block was further heated at 100°C in xylene to remove the insoluble crystalline propylene polymer block.

A-2 Polypropylene resin

Another propylene polymer component of the thermoplastic resin composition of the first preferred embodiment is a polypropylene resin.

The polypropylene resin is a homopolypropylene resin or a polypropylene resin which has a crystalline random copolymer moiety or a block copolymer moiety each comprising a propylene unit and a unit of α -olefin such as ethylene, butene-1, pentene-1, 4-methylpentene-1, hexene-1, octene-1, etc. The content of each copolymer moiety is 0 to 2 weight %, preferably 0 to 1 weight % based on the total amount of the polymer. A content exceeding 2 weight % is undesirable because the molded articles have a poor impact strength at low temperatures and a raised embrittle temperature.

The polypropylene resin has a melt flow rate (MFR) of 20 to 200 g/10 min, preferably 40 to 180 g/10 min when measured at 230°C under a load of 2.16 kgf. When the MFR is less than 20 g/10 min, the resin composition is less flowable. An MFR exceeding 200 g/10 min undesirably reduces the ductility of the resin composition.

A polypropylene resin having a high MFR can be directly produced by polymerization of the propylene monomer. However, in view of the productivity, the high MFR polypropylene resin is preferred to be produced by subjecting a polypropylene resin having a low MFR to a chain length regulating treatment in which a polypropylene resin having a low MFR is kneaded at 180 to 300°C for 1 to 10 minutes in the presence of a chain length regulator such as an organic peroxide, sulfur-containing compound, etc. to reduce the chain length, i.e., reduce the molecular weight.

The polypropylene resin of the present invention has a stereospecificity, represented by an isotactic pentad fraction (IPF), of 95% or more, preferably 97% or more. If IPF is less than 95%, the polypropylene resin is low in the crystallinity to give the molded articles having a poor stiffness and a low heat distortion temperature. The IPF is a fraction ratio of the number of five continuous propylene monomer units (pentad) bonded isotactically to the total number of five continuous propylene monomer units determined by a method described in A. Zambelli et al.; *Macromolecules*, **6**, 925 (1973) which includes measuring ^{13}C -NMR spectra. The assignment of each peak of ^{13}C -NMR spectra was made according to a method described in *Macromolecules*, **8**, 687 (1975). The IPF was calculated by dividing the peak intensity of mmmm peak by the total of the peak intensities of all the methyl carbons in the n-heptane insolubles of the polypropylene.

The above polypropylene resin may be produced by various known method, and preferably by polymerizing the propylene monomer in the presence of a stereo-specific polymerization catalyst by a known slurry polymerization, solution polymerization, liquid phase polymerization using olefin monomer as the medium, vapor phase polymerization, etc.

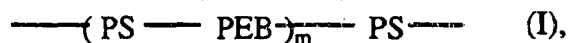
In a more specific example, the propylene monomer is polymerized in the presence of a catalyst system comprising a transition metal compound such as titanium trichloride, titanium tetrachloride, etc. alone or carried on a support mainly composed of a magnesium halide such as magnesium chloride, etc., and a organoaluminum compound such as triethylaluminum, diethylaluminum chloride, etc. After polymerizing the propylene monomer, the copolymer moiety (2 weight % or less) may be introduced by further polymerizing a comonomer. The copolymer moiety is random and the content thereof may be determined as cold xylene insolubles.

B Styrene-containing elastomer component

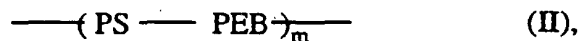
The second component of the thermoplastic resin composition of the first preferred embodiment is the styrene-containing elastomer component which is an elastomeric styrene-containing block copolymer or a binary elastomer which is a mixture of elastomeric styrene-containing block copolymers having different melt flow rates.

B-1 Elastomeric styrene-containing block copolymer

The elastomeric styrene-containing block copolymer is represented by the formula (I) or (II):



and



wherein PS is a polystyrene block, PEB is poly(ethylene-butene) block and m is an integer of 1 or more. The integer m is preferably 1 to 4, and more preferably 1 to 2.

The elastomeric styrene-containing block copolymer may be produced by block-copolymerizing a mono-vinylaromatic compound and a conjugated diene, and subsequently hydrogenating the resulting block copolymer. In the present invention, styrene and 1,3-butadiene are preferably used to obtain a block copolymer comprising a polystyrene block and a poly(ethylene-butene) block, and the block copolymer is then hydrogenated to produce the elastomeric styrene-containing block copolymer. It is preferable that 90 mol % or more of the aliphatic unsaturated bonds are hydrogenated, and an elastomeric styrene-containing block copolymer having no aliphatic unsaturated bond is preferably used in the present invention in view of weathering resistance and easy recycling of the wasted molded articles.

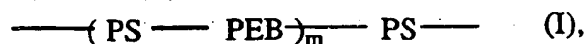
Of the elastomeric styrene-containing block copolymers represented by the formulae (I) and (II), preferred are those having two or more blocks consisting of the PS block and the PEB block, and more preferred are those having three or more blocks consisting of the PS block, the PEB block and the PS block. These elastomers are so-called as a styrene-ethylene-butene block copolymer elastomer (SEB) or a styrene-ethylene-butene-styrene copolymer elastomer (SEBS).

The elastomeric styrene-containing block copolymer has an MFR of 0.5 to 40 g/10 min, preferably 0.5 to 30 g/10 min. If the MFR is less than 0.5 g/10 min, the moldability is deteriorated due to insufficient fluidity of the resin composition, and the impact strength of the molded articles is poor. On the other hand, an MFR exceeding 40 g/10 min results in a poor ductility of the resin composition and insufficient impact strength of the molded articles.

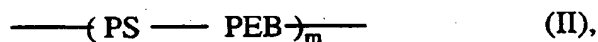
The styrene-containing elastomer component is contained in the resin composition in an amount of 10 to 30 weight %, preferably 10 to 25 weight % based on the total of the components (A), (B) and (C). If the content is less than 10 weight %, the impact strength of the molded articles is poor, and mechanical strength, stiffness, heat resistance and hardness of the molded articles are reduced when exceeding 30 weight %.

B-2 Binary elastomer

Each of the elastomeric styrene-containing block copolymer (a) and the elastomeric styrene-containing block copolymer (b) constituting the binary elastomer is represented by the following formula (I) or (II):



and



wherein PS is a polystyrene block, PEB is poly(ethylene-butene) block and m is an integer of 1 or more.

In the elastomeric styrene-containing block copolymer (a), the integer m is preferably 1 to 4, and more preferably 1 to 2, and the content of PS is 10 to 30 weight %, preferably 25 to 30 weight %. The MFR is 0.5 to 3 g/10 min, preferably 1 to 3 g/10 min.

In the elastomeric styrene-containing block copolymer (b), the content of PS is 10 to 30 weight %, preferably 10 to 24 weight %. The integer m is preferably 1 to 4, and more preferably 1 to 2. The MFR of the elastomeric styrene-containing block copolymer (b) is 4 to 100 g/10 min, preferably 5 to 30 g/10 min.

Like the elastomeric styrene-containing block copolymer described in paragraph B-1, the elastomeric styrene-containing block copolymers (a) and (b) are also preferred to have a structure of -PS-PEB- (SEB) or -PS-PEB-PS- (SEBS), and produced by copolymerization and a subsequent hydrogenation.

The MFR of each elastomeric styrene-containing block copolymer may be controlled to the respective range by suitably selecting the amount of the polymerization initiator.

The weight ratio of the elastomeric styrene-containing block copolymers (a) and (b) in the binary elastomer ((a) : (b)) is 40 to 80 : 20 to 60, preferably 50 to 75 : 25 to 50. If the ratio is outside the above range, the ductility and impact strength would be deteriorate and the brittle temperature would be raised. In addition, the difference of MFR (MFR(b) - MFR(a)) is preferably 3 g/10 min or more, more preferably 5 to 20 g/10 min in view of improving the impact strength and preventing the brittle temperature from being raised.

Also, the binary elastomer may contain two or more of the elastomeric styrene-containing block copolymers (a) and/or two or more of the elastomeric styrene-containing block copolymers (b).

The binary elastomer component is contained in the resin composition in an amount of 5 to 30 weight %, preferably

10 to 25 weight % based on the total of the components (A), (B) and (C). If the content is less than 5 weight %, the impact strength of the molded articles is poor, and mechanical strength, stiffness, heat resistance and hardness of the molded articles are reduced when exceeding 30 weight %.

5 C Talc

Talc used in the present invention is characterized by an average particle size of 5 μm or less, preferably 3 to 5 μm , measured by a particle size distribution analyzer utilizing laser diffraction and scattering. If the average particle size exceeds 5 μm , the molded articles are insufficient in the stiffness and the dimension stability. The talc is preferred to be surface-treated by a modified silicone, titanate coupling agent, etc., because such a treatment improves the stiffness and the heat resistance of the molded articles. The talc is contained 10 to 40 weight %, preferably 10 to 30 weight % based on the total of the components (A), (B) and (C). If the content is less than 10 weight %, the stiffness and the heat resistance of the molded articles are poor, and the ductility of the resin composition is reduced when exceeds 40 weight %.

15 D Other Additives

The thermoplastic resin composition of the present invention may contain an antioxidant, heat stabilizer and light stabilizer, respectively in an amount of 0.05 to 2 parts by weight based on 100 parts by weight of the total of the above components (A), (B) and (C), according to the application use such as inner lining or outer lining material for automobiles. If the amount is less than 0.05 parts, no detectable effect would be obtained. No additional effect would be obtained if an amount exceeding 2 parts is added, and in addition, the properties of the resin composition would be deteriorated.

The phenol-type antioxidant may include tetrakis[methylene-3(3,5-di-t-butyl-4-hydroxyphenyl)propionate]methane, 2,6-di-t-butyl-4-methylphenol, tris(3,5-di-t-butyl-4-hydroxyphenyl) isocyanurate, etc. The phosphorus-containing antioxidant may include tris(2,4-di-t-butylphenyl) phosphite, 4,4'-butylidene-bis(3-methyl-6-t-butylphenyl-di-tridecyl) phosphite, 1,1,3-tris(2-methyl-4-ditridecyl-phosphite-5-t-butyl), etc.

The heat stabilizer may include a sulfur-containing compound such as distearyl thiopropionate, dilauryl thiopropionate, etc.

The light stabilizer may include bis(2,2,6,6-tetramethyl-4-piperidine) sebacate, a condensate of succinic acid and dimethyl-1-(2-hydroxyethyl)-4-hydroxyl-2,2,6,6-tetramethylpiperidine, poly[6-(1,1,3,3-tetramethylbutyl)amino-1,3,5-triazine-2,4-diyl][(2,2,6,6-tetramethyl-4-piperidyl)imino]hexamethylene[(2,2,6,6-tetramethyl-4-piperidyl)imino], a condensate of N,N'-bis(3-aminopropyl)ethylenediamine-2,4-bis[N-butyl-N-(1,2,2,6,6-pentamethyl-4-piperidyl)amino]-6-chloro-1,3,5-triazine, etc.

The resin composition of the present invention may further contain other additives such as a releasing agent, an antistatic agent, a plasticizer, a fire retardant, a lubricant, an anti-copper-damage agent, an organic or inorganic pigment and a dispersant therefor, etc. to improve the properties of the resin composition according to the application use.

These additives are usually added at the time of mixing the essential components (A), (B) and (C). Also, the additives may be post-blended in the injection molding step as a masterbatch containing the additives in a high concentration.

The thermoplastic resin composition of the present invention may be produced by dry-blending the essential components and the optional additives, and then melt-kneading the blend at 180 to 300°C preferably 190 to 210°C in a single-screw extruder, a twin-screw extruder, Banbury mixer, a kneader, etc. The resin composition thus produced has an MFR of 20 to 50 g/10 min, preferably 25 to 35 g/10 min.

45 [2] SECOND THERMOPLASTIC RESIN COMPOSITION

The second preferred thermoplastic resin composition of the present invention contains (A) a first propylene polymer component having a relatively low melt flow rate, (B) a second propylene polymer component having a relatively high melt flow rate, (C) a styrene-containing elastomer component, and (D) talc as the essential components.

A First propylene polymer component

The first propylene polymer component is at least one selected from the group consisting of a first homopolypropylene and a first ethylene-propylene block copolymer, and is contained 10 to 50 weight %, preferably 10 to 40 weight % based on the total weight of the components (A), (B), (C) and (D). If the content is less than 10 weight %, the stiffness, heat resistance and hardness of the molded articles are poor, and mechanical strength and ductility are reduced when exceeding 50 weight %.

A-1 First homopolypropylene

The first homopolypropylene has a relatively low melt flow rate and may include a crystalline random copolymer and block copolymer each containing, as a copolymerized component, for example, an α -olefin such as ethylene, butene-1, pentene-1, 4-methylpentene-1, heptene-1, hexene-1, octene-1, etc. in a small amount up to about 1 weight %.

The first homopolypropylene has a melt flow rate (MFR) of 2 to 30 g/10 min, preferably 2 to 20 g/10 min when measured at 230°C under a load of 2.16 kgf. When the MFR is less than 2 g/10 min, the resin composition is less flowable. An MFR exceeding 30 g/10 min undesirably reduces the ductility of the resin composition.

The isotactic pentad fraction (IPF) of the first homopolypropylene is preferably more than 95%, more preferably 97% or more.

The above first homopolypropylene may be produced by various known method, and preferably by polymerizing the propylene monomer in the presence of a stereo-specific polymerization catalyst by a known slurry polymerization, solution polymerization, liquid phase polymerization using olefin monomer as the medium, vapor phase polymerization, etc.

In a more specific example, the propylene monomer is polymerized in the presence of a catalyst system comprising a transition metal compound such as titanium trichloride, titanium tetrachloride, etc. alone or carried on a support mainly composed of a magnesium halide such as magnesium chloride, etc., and a organoaluminum compound such as triethylaluminum, diethylaluminum chloride, etc. After polymerizing the propylene monomer, the copolymer moiety (1 weight % of less) may be formed by further polymerizing a comonomer. The copolymer moiety is random and the amount thereof may be determined as the cold xylene insolubles. Also, the first homopolypropylene may be produced by a reactor blend utilizing a multi-stage homopolymerization of propylene.

A-2 First ethylene-propylene block copolymer

The first ethylene-propylene block copolymer has an MFR of 2 to 30 g/10 min, preferably 2 to 20 g/10 min. When the MFR is less than 2 g/10 min, the resin composition is less flowable and the moldability, in particular, the injection moldability is deteriorated. An MFR exceeding 30 g/10 min undesirably reduces the mechanical strength of the molded articles. The isotactic pentad fraction (IPF) of the first ethylene-propylene block copolymer is preferably 95% or more, more preferably 97% or more. The other properties of the first ethylene-propylene block copolymer is the same as those of the ethylene-propylene block copolymer for the first preferred embodiment.

Also, the first ethylene-propylene block copolymer may be produced in the same method as described in the production of the ethylene-propylene block copolymer for the first preferred embodiment.

B Second propylene polymer component

The second propylene polymer component is at least one selected from the group consisting of a second homopolypropylene and a second ethylene-propylene block copolymer, and is contained 10 to 50 weight %, preferably 10 to 40 weight % based on the total weight of the components (A), (B), (C) and (D). If the content is less than 10 weight %, the stiffness, heat resistance and hardness of the molded articles are poor, and mechanical strength and ductility are reduced when exceeding 50 weight %. The total amount of the first propylene polymer component and the second propylene polymer component is preferably 30 to 80 weight % based on the total weight of the components (A), (B), (C) and (D).

B-1 Second homopolypropylene

The second homopolypropylene is basically the same as the first homopolypropylene except for having an MFR of 50 to 1000 g/10 min, preferably 100 to 600 g/10 min. When the MFR is less than 50 g/10 min, the resin composition is less flowable. An MFR exceeding 1000 g/10 min undesirably reduces the ductility of the resin composition and the mechanical strength of the molded articles. The second homopolypropylene may be produced in the same method as described in the production of the first homopolypropylene.

The MFR of the second homopolypropylene may be regulated within the specified range by a chain-length regulating treatment, in which a homopolypropylene having a relatively low MFR is kneaded in an extruder at 180 to 300°C for 1 to 10 minutes in the presence of a chain-length regulator such as an organic peroxide, a sulfur-containing compound, etc. to reduce the molecular weight of the homopolypropylene. The organic peroxide may include t-butyl hydroperoxide, dicumyl peroxide, di-t-butyl peroxide, benzoyl peroxide, 2,5-dimethyl-2,5-di(t-butylperoxy)hexane, 2,5-dimethyl-2,5-di(t-butylperoxy)hexyne-3, methyl ethyl ketone peroxide, etc. Of the above peroxides, preferred are 2,5-dimethyl-2,5-di(t-butylperoxy)hexane and 2,5-dimethyl-2,5-di(t-butylperoxy)hexyne-3. As the sulfur-containing compound, triauryl trithiophosphite, tristearyl trithiophosphite, etc. may be used. The chain-length regulator is selected

according to the desired MFR range, and usually 0.001 to 2 parts by weight based on 100 parts by weight of a homopolypropylene being treated is used directly or in the form of masterbatch. By such a treatment, the second homopolypropylene having a MFR within the specified range can be easily obtained with a minimum loss of the monomer to improve the productivity, and also, the second homopolypropylene thus produced enhances the mechanical strength of the molded articles. The chain-length regulating treatment is also applicable to producing the first homopolypropylene.

B-2 Second ethylene-propylene block copolymer

The second ethylene-propylene block copolymer has an MFR of 50 to 1000 g/10 min, preferably 100 to 600 g/10 min. When the MFR is less than 50 g/10 min, the resin composition is less flowable. An MFR exceeding 1000 g/10 min undesirably reduces the ductility of the resin composition and the mechanical strength of the molded articles. The MFR may be regulated within the specified range by the chain-length regulating treatment described above. This treatment is also applicable to regulating the MFR of the first ethylene-propylene block copolymer. The other properties of the second ethylene-propylene block copolymer is the same as those of the ethylene-propylene block copolymer for the first preferred embodiment.

The isotactic pentad fraction (IPF) of the second ethylene-propylene block copolymer is preferably 95% or more, more preferably 97% or more.

Also, the second ethylene-propylene block copolymer may be produced in the same method as described in the production of the ethylene-propylene block copolymer for the first preferred embodiment.

C Styrene-containing elastomer component

The styrene-containing elastomer component is the same elastomeric styrene-containing block copolymer as described in the paragraph B-1 for the first preferred embodiment, and is contained 10 to 30 weight %, preferably 10 to 25 weight % based on the total weight of the components (A), (B), (C) and (D). If the content is less than 10 weight %, the impact strength of the molded articles is poor, and the mechanical strength, stiffness, heat resistance and hardness of the molded articles are reduced when exceeding 30 weight %.

D Talc

The talc used here is the same as that used in the first preferred embodiment, and added 10 to 40 weight %, preferably 10 to 30 weight % based on the total weight of the components (A), (B), (C) and (D). If the content is less than 10 weight %, the stiffness and the heat resistance of the molded articles are poor, and the ductility is reduced when exceeds 40 weight %.

E Other Additives

The same additives as used in the first preferred embodiment may be used in a respective amount of 0.05 to 2 parts by weight based on 100 parts by weight of the total of the above components (A), (B), (C) and (D).

The thermoplastic resin composition of the second preferred embodiment may be produced from the above ingredients in the same manner as in producing the first preferred embodiment. The second resin composition thus produced has an MFR of 20 to 50 g/10 min, preferably 25 to 35 g/10 min.

[3] THIRD THERMOPLASTIC RESIN COMPOSITION

The third preferred thermoplastic resin composition of the present invention contains (A) a first propylene polymer component having a relatively low melt flow rate, (B) a second propylene polymer component having a relatively high melt flow rate, (C) a styrene-containing elastomer component, and (D) talc as the essential components.

A First propylene polymer component

The first propylene polymer component is at least one selected from the group consisting of a first homopolypropylene and an ethylene-propylene random copolymer, and is contained 10 to 50 weight %, preferably 10 to 40 weight % based on the total weight of the components (A), (B), (C) and (D). If the content is less than 10 weight %, the ductility of the resin composition is poor, and the stiffness and heat resistance are reduced when exceeding 50 weight %.

A-1 First homopolypropylene

The first homopolypropylene for the third preferred embodiment is characterized by having an isotactic pentad fraction (IPF) of 90 to 95%, preferably 92 to 95%. If the IPF is less than 90%, the crystallinity of the first homopolypropylene is too low; this resulting in a poor stiffness and a raised heat distortion temperature of the molded articles.

The other properties of the first homopolypropylene is the same as those of the first homopolypropylene for the second preferred embodiment. Namely, the first homopolypropylene for the third preferred embodiment has a melt flow rate (MFR) of 2 to 30 g/10 min, preferably 2 to 20 g/10 min, and may include a crystalline random copolymer and block copolymer each containing a copolymerized component, for example, an α -olefin such as ethylene, butene-1, pentene-1, 4-methylpentene-1, heptene-1, hexene-1, octene-1, etc. in a small amount up to about 1 weight %.

A-2 Ethylene-propylene random copolymer

The ethylene-propylene random copolymer contains the ethylene unit in an amount of 0.1 to 1 weight % based on the copolymer. If the ethylene content is less than 0.1 weight %, the ductility of the resin composition would be poor, and a content exceeding 1 weight % results in a poor stiffness and a raised heat distortion temperature.

The MFR of the ethylene-propylene random copolymer is 2 to 30 g/10 min, preferably 2 to 20 g/10 min. When the MFR is less than 2 g/10 min, the resin composition is less flowable, and an MFR exceeding 30 g/10 min results in an insufficient ductility of the resin composition.

B Second propylene polymer component

The second propylene polymer component is a second homopolypropylene, and is contained 10 to 50 weight %, preferably 20 to 50 weight % based on the total weight of the components (A), (B), (C) and (D). If the content is less than 10 weight %, the stiffness, heat resistance and hardness of the molded articles are poor, and mechanical strength and ductility are reduced when exceeding 50 weight %. The total amount of the first propylene polymer component and the second propylene polymer component is preferably 30 to 80 weight % based on the total weight of the components (A), (B), (C) and (D).

The second homopolypropylene is the same as the second homopolypropylene used in the second preferred embodiment, namely, has an MFR of 50 to 1000 g/10 min, preferably 100 to 600 g/10 min, and an IPF of 95% or more, preferably 97% or more.

C Styrene-containing elastomer component

The styrene-containing elastomer component is the same elastomeric styrene-containing block copolymer as described in the paragraph B-1 for the first preferred embodiment, and is contained 10 to 30 weight %, preferably 10 to 25 weight % based on the total weight of the components (A), (B), (C) and (D). If the content is less than 10 weight %, the impact strength of the molded articles is poor, and the mechanical strength, stiffness, heat resistance and hardness of the molded articles are reduced when exceeding 30 weight %.

D Talc

The talc used here is the same as that used in the first preferred embodiment, and added 10 to 40 weight %, preferably 10 to 30 weight % based on the total weight of the components (A), (B), (C) and (D). If the content is less than 10 weight %, the stiffness and the heat resistance of the molded articles are poor, and the ductility is reduced when exceeds 40 weight %.

E Other Additives

The same additives as used in the first preferred embodiment may be used in a respective amount of 0.05 to 2 parts by weight based on 100 parts by weight of the total of the above components (A), (B), (C) and (D).

The thermoplastic resin composition of the third preferred embodiment may be produced from the above ingredients in the same manner as in producing the first preferred embodiment. The second resin composition thus produced has an MFR of 20 to 50 g/10 min, preferably 25 to 35 g/10 min.

The present invention will be further described while referring to the following Examples which should be considered to illustrate various preferred embodiments of the present invention. In the following examples and comparative examples, the propylene polymer components and the elastomer components shown below were used.

Ethylene-propylene block copolymer (BPP):

BJ715, BJ730X, TBJ580X6, BJ780, BJ790 and BJ540, all manufactured by Tonen Chemical Corporation.

Styrene-ethylene-butene-styrene copolymer (SEBS):

G1052, G1650, G1652, G1657 and G1701 all manufactured by Shell Chemical Co., and H1031, H1041, H1042, H1052, H1071 all manufactured by Asahi Chemical Industry Co., Ltd.

Styrene-ethylene-propylene-styrene copolymer (SEPS):

K203 manufactured by Kuraray Co., Ltd.

Styrene-ethylene-propylene-styrene copolymer (SEP)

G1701 manufactured by Shell Chemical Co.

Ethylene-propylene copolymer rubber (EPR)

EP961SP (MFR=0.8 g/10 min, ethylene content: 77 weight %) manufactured by Japan Synthetic Rubber Co., Ltd.

Ethylene-butene copolymer rubber (EBR)

EBM2011P (MFR=1 g/10 min, ethylene content: 80 weight %) manufactured by Japan Synthetic Rubber Co., Ltd.

EXAMPLES 1 to 10, and COMPARATIVE EXAMPLES 1 to 7

The ingredients of the thermoplastic resin composition used here are shown below.

[1] Ethylene-propylene block copolymer (BPP)

Table 1

Properties	BPP-1	BPP-2	BPP-3	BPP-4	BPP-5	BPP-6
MFR ⁽¹⁾ (g/10 min)	34	85	85	110	40	20*
C _v ⁽²⁾ (wt. %)	11	9	9	9	13	10
G _v ⁽³⁾ (wt. %)	42	35	50	36	50	40
[η] _{CXS} ⁽⁴⁾ (dl/g)	5.0	5.3	5.0	4.8	3.5	4.0

Note: (*): Outside the range specified in the present invention.

(1): MFR measured at 230°C under a load of 2.16 kgf according to ASTM D1238.

(2): C_v is the content of the ethylene-propylene copolymer block (cold xylene solubles) in the ethylene-propylene block copolymer.

(3): G_v is the ethylene content in the ethylene-propylene copolymer block (cold xylene solubles).

(4): [η]_{CXS} is the intrinsic viscosity of the ethylene-propylene copolymer block (cold xylene solubles).

[2] SEBS and other elastomers

Table 2 (to be contd.)

Properties	SEBS-1	SEBS-2	SEBS-3	SEBS-4	SEBS-5	SEBS-6
MFR ⁽⁵⁾ (g/10 min)	8	2	0.1*	5	30	12
PS ⁽⁶⁾ (wt. %)	13	29	29	30	20	20

Table 2 (contd.)

Properties	SEBS-7	SEBS-8	SEP	SEPS	EPR	EBR
MFR ⁽¹⁾ (g/10 min)	0.5	160*	0.5	0.5	0.8	1
PS ⁽²⁾ (wt. %)	20	30	37	13	-	-

Note: (*): Outside the range specified in the present invention.

(1): MFR measured at 230°C under a load of 2.16 kgf according to ASTM D1238.

(2): PS is the content of the polystyrene block in each of SEBS, SEP and SEPS.

[3] Talc

Talc having an average particle size of 1.2 µm (LMS300 manufactured by Fiji Talc K.K.) was used.

[4] Additives

The following additives were used.

Antioxidant-1: Irganox 1010 manufactured by Ciba-Geigy AG.

Antioxidant-2: Mark 2112 manufactured by Asahi Denka K.K.

Heat Stabilizer: Sumilizer TPS manufactured by Sumitomo Chemical Company, Ltd.

Light Stabilizer: Chimassorb 944 manufactured by Ciba-Geigy AG.

Each BPP, SEBS or other elastomer, the talc and the additives shown above were mixed in respective blending ratio shown in Table 3. After adding the antioxidant-1, antioxidant-2, heat stabilizer, and light stabilizer, each in an amount of 0.2 part by weight, to each 100 parts by weight of the mixture, the resulting mixture was dry-blended in a super mixer, melt-kneaded in a twin-screw extruder (PCM-45 manufactured by Ikegai K.K., L/D=32) at 200°C and 200 rpm, and then extruded into the form of pellets to produce each thermoplastic resin composition.

Each resin composition was injection-molded by an injection molding machine (IS-90B manufactured by Toshiba Machine Co. Ltd.) under the conditions of the cylinder temperature of 210°C and the mold temperature of 50°C to produce each test specimen which was subjected to the following tests for evaluating the physical properties of the molded article. The results are shown in Table 3.

Table 3 (to be contd.)

	Examples					
	1	2	3	4	5	6
Composition						
BPP						
Kind	BPP-1	BPP-2	BPP-3	BPP-4	BPP-5	BPP-2
Blend ratio (wt. %)	64	63	63	63	65	63
Elastomer						
Kind	SEBS-1	SEBS-2	SEBS-2	SEBS-2	SEBS-2	SEBS-1
Blend ratio (wt. %)	16	17	17	17	15	17
Talc						
Blend ratio (wt. %)	20	20	20	20	20	20
Properties						
MFR ⁽¹⁾ (g/10 min)	25	31	32	45	22	41
Tensile strength ⁽²⁾ (kg/cm ²)	252	242	242	240	253	230

Elongation at break ⁽³⁾ (%)	500	600	300	300	600	300
Bending modulus ⁽⁴⁾ (kg/cm ²)	22400	25000	24700	24000	22600	22500
Bending strength ⁽⁵⁾ (kg/cm ²)	354	350	350	350	360	351
Izod impact strength ⁽⁶⁾ (kg-cm/cm)	28	26	24	23.5	28	31
Heat distortion temperature ⁽⁷⁾ (°C)	80	74	74	74	75	77
Rockwell hardness ⁽⁸⁾	70	76	75	75	74	70

Table 3 (contd.)

	Examples				Comparative Examples	
	7	8	9	10	1	2
<u>Composition</u>						
BPP						
Kind	BPP-2	BPP-2	BPP-2	BPP-2	BPP-6	BPP-2
Blend ratio (wt. %)	63	63	63	63	64	60
Elastomer						
Kind	SEBS-4	SEBS-5	SEBS-6	SEBS-7	SEBS-1	EPR/EBR
Blend ratio (wt. %)	17	17	17	17	16	10/10
Talc						
Blend ratio (wt. %)	20	20	20	20	20	20
<u>Properties</u>						
MFR ⁽¹⁾ (g/10 min)	37	49	40	31	17	25
Tensile strength ⁽²⁾ (kg/cm ²)	246	235	238	235	260	236
Elongation at break ⁽³⁾ (%)	300	300	300	500	600	600
Bending modulus ⁽⁴⁾ (kg/cm ²)	22500	22300	22500	23200	23500	24000
Bending strength ⁽⁵⁾ (kg/cm ²)	366	351	356	356	350	340
Izod impact strength ⁽⁶⁾ (kg-cm/cm)	20	26	30	20	35	18.5
Heat distortion temperature ⁽⁷⁾ (°C)	76	76	75	75	78	79
Rockwell hardness ⁽⁸⁾	79	71	74	77	70	76

Table 3 (contd.)

	Comparative Examples				
	3	4	5	6	7
Composition					
BPP					
Kind	BPP-2	BPP-2	BPP-2	BPP-2	BPP-2
Blend ratio (wt. %)	60	63	63	63	63
Elastomer					
Kind	EPR	SEBS-3	SEP	SEPS	SEBS-8
Blend ratio (wt. %)	20	17	17	17	17
Talc					
Blend ratio (wt. %)	20	20	20	20	20
Properties					
MFR ⁽¹⁾ (g/10 min)	24	20	21	30	71
Tensile strength ⁽²⁾ (kg/cm ²)	226	237	217	223	257
Elongation at break ⁽³⁾ (%)	220	500	15	300	50
Bending modulus ⁽⁴⁾ (kg/cm ²)	22100	24000	22000	23000	23500
Bending strength ⁽⁵⁾ (kg/cm ²)	333	358	322	333	380
Izod impact strength ⁽⁶⁾ (kg-cm/cm)	18.8	12	30	15	8
Heat distortion temperature ⁽⁷⁾ (°C)	70	77	74	76	73
Rockwell hardness ⁽⁸⁾	68	79	73	74	78

- Note: (1): MFR measured at 230°C under a load of 2.16 kgf according to ASTM D1238.
 (2): Tensile strength was measured according to ASTM D638.
 (3): Elongation at break was measured according to ASTM D638.
 (4): Bending modulus was measured according to ASTM D790.
 (5): Bending strength was measured according to ASTM D790.
 (6): Izod impact strength was measured at 23°C according to ASTM D256.
 (7): Heat distortion temperature was measured under a

load of 18.6 kgf/cm² according to ASTM D648.
 (8): Rockwell hardness was measured according to ASTM
 D785 (R scale).

As seen from the results, each resin composition of Examples 1 to 10 had an MFR showing a good fluidity and well-balanced mechanical properties. On the other hand, in Comparative Examples 1 to 7, the MFR was low (insufficient fluidity) when the mechanical properties were rather well balanced, or the mechanical properties were not balanced when the composition was well flowable. Further, the composition containing a styrene-containing elastomer (SEP or SEPS) other than those specified in the present invention and the composition containing an olefin elastomer (EPR and EBR) were insufficient in ductility and impact strength.

EXAMPLES 11 to 20 and COMPARATIVE EXAMPLES 8 to 11

The ingredients of the thermoplastic resin composition used here are shown below.

[1] Polypropylene Resin (PP)

Table 4

Properties	PP-1	PP-2	PP-3	PP-4	PP-5	PP-6	PP-7	PP-8
MFR ⁽¹⁾ (g/10 min)	40	70	90	140	40	85	85	20
IPF ⁽²⁾ (%)	97.7	98.0	97.6	97.6	95.0	97.0	97.0	97.3
C _v ⁽³⁾ (wt. %)	0	0	0	0	0	2	9*	0

Note: (*): Outside the range specified in the present invention.

(1): MFR measured in the same manner as above.

(2): IPF is an isotactic pentad fraction measured by ¹³C-NMR.

(3): C_v is the content of the copolymer block (cold xylene solubles) in the polypropylene resin.

The MFR of each of PP-2 to PP-4 was regulated to the respective value by subjecting PP-1 to a chain-length regulating treatment.

[2] SEBS and other elastomers

Table 5

Properties	SEBS-9	SEBS-10	SEBS-11	SEBS-12	SEBS-13	SEPS	EPR
MFR ⁽¹⁾ (g/10 min)	1.6	30	12	5	160*	0.5	0.8
PS ⁽²⁾ (wt. %)	29	20	20	30	30	13	-

Note: (*): Outside the range specified in the present invention.

(1) and (2) are the same as in Table 2.

[3] Talc

The same talc as in Examples 1 to 10 was used.

[4] Additives

The same additives as in Examples 1 to 10 were used.

The resin compositions and the test specimens were produced in the same manner as in Examples 1 to 10. The physical properties measured on each specimen are shown in Table 6.

Table 6 (to be contd.)

Composition	Examples				
	11	12	13	14	15
PP					
Kind	PP-1	PP-2	PP-2	PP-3	PP-4
Blend ratio (wt. %)	57	58	57	57	57
Elastomer					
Kind	SEBS-9	SEBS-9	SEBS-9	SEBS-9	SEBS-9
Blend ratio (wt. %)	23	22	23	23	23
Talc					
Blend ratio (wt. %)	20	20	20	20	20
Properties					
MFR ⁽¹⁾ (g/10 min)	22	37	34	27	31
Tensile strength ⁽²⁾ (kg/cm ²)	230	235	229	226	233
Elongation at break ⁽³⁾ (%)	600	400	500	600	500
Bending modulus ⁽⁴⁾ (kg/cm ²)	21400	21900	21200	22500	24500
Bending strength ⁽⁵⁾ (kg/cm ²)	346	345	335	347	369

Izod impact strength ⁽⁶⁾ (kg-cm/cm)					
at 23°C	42	29	38	36	28
at -30°C	4.1	3.8	4.0	4.1	3.6
Heat distortion temperature ⁽⁷⁾ (°C)	73	74	73	74	77
Rockwell hardness ⁽⁸⁾	75	74	72	76	79
Embrittle temperature ⁽⁹⁾ (°C)	-20	-12	-15	-15	-13

Table 6 (contd.)

Examples					
	16	17	18	19	20
<u>Composition</u>					
PP					
Kind	PP-5	PP-6	PP-1	PP-1	PP-1
Blend ratio (wt. %)	58	59	59	60	58
Elastomer					
Kind	SEBS-9	SEBS-9	SEBS-10	SEBS-11	SEBS-12
Blend ratio (wt. %)	22	21	21	20	22
Talc					
Blend ratio (wt. %)	20	20	20	20	20
<u>Properties</u>					
MFR ⁽¹⁾ (g/10 min)	22	36	33	26	21
Tensile strength ⁽²⁾ (kg/cm ²)	266	226	238	241	264
Elongation at break ⁽³⁾ (%)	450	500	400	600	450
Bending modulus ⁽⁴⁾ (kg/cm ²)	22800	21300	23000	21300	22500
Bending strength ⁽⁵⁾ (kg/cm ²)	388	379	352	355	384
Izod impact strength ⁽⁶⁾ (kg-cm/cm)					
at 23°C	23	37	26	33	22
at -30°C	3.7	3.8	3.6	3.8	3.6
Heat distortion temperature ⁽⁷⁾ (°C)	75	72	74	75	74
Rockwell hardness ⁽⁸⁾	74	70	72	72	76
Embrittle temperature ⁽⁹⁾ (°C)	-13	-12	-12	-20	-12

Table 6 (contd.)

	Comparative Examples			
	8	9	10	11
Composition				
PP				
Kind	PP-7	PP-8	PP-1	PP-1
Blend ratio (wt. %)	62	60	57	57
Elastomer				
Kind	SEBS-9	SEBS-13	SEPS	EPR
Blend ratio (wt. %)	18	20	23	23
Talc				
Blend ratio (wt. %)	20	20	20	20
Properties				
MFR ⁽¹⁾ (g/10 min)	33	37	11.5	13.6
Tensile strength ⁽²⁾ (kg/cm ²)	230	256	220	235
Elongation at break ⁽³⁾ (%)	600	100	30	600
Bending modulus ⁽⁴⁾ (kg/cm ²)	23400	21400	24000	23100
Bending strength ⁽⁵⁾ (kg/cm ²)	348	367	360	368
Izod impact strength ⁽⁶⁾ (kg-cm/cm)				
at 23°C	26	9	7	22
at -30°C	3.0	2.1	2.5	3.5
Heat distortion temperature ⁽⁷⁾ (°C)	74	70	75	77
Rockwell hardness ⁽⁸⁾	76	74	78	72
Embrittle temperature ⁽⁹⁾ (°C)	-10	-4	0	-3

Note: (1) to (5), and (7) to (8) are the same as in Table 3.

(6) Izod impact strength was measured at 23°C and -30°C according to ASTM D256.

(9) Embrittle temperature was measured according to ASTM D746.

As seen from the results, each resin composition of Examples 11 to 20 had an MFR showing a good fluidity and well-balanced mechanical properties. On the other hand, the comparative composition containing a polypropylene resin having an copolymer block content exceeding 2 weight % was deteriorated in the impact strength at a low temperature and had a high brittle temperature. Further, the comparative composition containing a styrene-containing

elastomer having an MFR outside the range of the present invention or an elastomer (SEPS and EPR) other than those specified in the present invention was insufficient in the ductility and impact strength and had a high brittle temperature.

EXAMPLE 21 to 24 and COMPARATIVE EXAMPLES 12 to 13

The ingredients of the thermoplastic resin composition used here are shown below.

[1] Ethylene-propylene block copolymer (BPP)

Table 7

Properties	BPP-7	BPP-8
MFR ⁽¹⁾ (g/10 min)	85	85
C _v ⁽²⁾ (wt. %)	9	9
G _v ⁽³⁾ (wt. %)	50	35
[η] _{CXS} ⁽⁴⁾ (dl/g)	5.0	5.3

Note: (1) to (4) are the same as in Table 1.

[2] SEBS and other elastomers

Table 8

Properties	SEBS-14	SEBS-15	SEBS-16	SEBS-17	SEPS	EPR
MFR ⁽¹⁾ (g/10 min)	1.6	8	5	12	0.5	0.8
PS ⁽²⁾ (wt. %)	29	13	30	20	13	-

Note: (1) and (2) are the same as in Table 2.

[3] Talc

Talc having an average particle size of 3.6 μm (AT164 manufactured by Asada Seifun K.K.) was used.

[4] Additives

The same additives as in Examples 1 to 10 were used.

The resin compositions and the test specimens were produced in the same manner as in Examples 1 to 10. The physical properties measured on each specimen are shown in Table 9.

Table 9

	Examples				Comparative Examples	
	21	22	23	24	12	13
Composition						
BPP						
Kind						
Blend ratio (wt. %)	BPP-7 61	BPP-7 63	BPP-7 61	BPP-7 61	BPP-8 63	BPP-8 60
Elastomer						
Kind						
Blend ratio (wt. %)	SEBS-14/SEBS-15 9.5/9.5	SEBS-14/SEBS-15 8.5/8.5	SEBS-14/SEBS-16 9.5/9.5	SEBS-14/SEBS-17 9.5/9.5	SEPS 17	EPR 20
Talc						
Blend ratio (wt. %)	20	20	20	20	20	20
Properties						
MFR ⁽¹⁾ (g/10 min)	38	40	34	38	30	24
Tensile strength ⁽²⁾ (kg/ cm ²)	236	249	236	233	223	226
Elongation at break ⁽³⁾ (%)	600	480	500	480	300	220
Bending modulus ⁽⁴⁾ (kg/ cm ²)	22600	23600	22000	23000	23000	22100
Bending strength ⁽⁵⁾ (kg/ cm ²)	342	363	343	343	333	333
Izod impact strength ⁽⁶⁾ (kg.cm/cm)						
at 23°C	36.0	30.0	34.1	33.3	15.0	18.8
at -30°C	4.1	3.2	3.9	4.4	3.0	3.2
Heat distortion temperature ⁽⁷⁾ (°C)	80	83	79	78	76	70
Rockwell hardness ⁽⁸⁾	74	77	75	73	74	68
Embrittle temperature ⁽⁹⁾ (°C)	-20	-15	-16	-18	-5	-2

Note: (1) to (5) and (7) to (8) are the same as in Table 3, and (6) and (9) are the same as in Table 6.

As seen from the results, each resin composition of Examples 21 to 24 had an MFR showing a good fluidity and well-balanced mechanical properties. Since the comparative composition contains SEPS or EPR in place of a binary elastomer of the present invention, the mechanical properties were not well balanced, in particular, the comparative examples were insufficient in the ductility, impact strength and tensile properties, and had a raised brittle temperature.

EXAMPLES 25 to 33 and COMPARATIVE EXAMPLES 14 to 16

The ingredients of the thermoplastic resin composition used here are shown below.

[1] Polypropylene Resin (PP)

Table 10

Properties	PP-9	PP-10	PP-11	PP-12	PP-13
MFR ⁽¹⁾ (g/10 min)	80	100	60	150	180
IPF ⁽²⁾ (%)	97.3	97.2	97.7	97.0	96.8
C _v ⁽³⁾ (wt. %)	0	0	0	0	0

Note: (1) to (3) are the same as in Table 4.

The MFR of each of PP-9 to PP-13 was regulated to the respective value by subjecting a homopolypropylene having an MFR of 40 g/10 min to a chain length regulating treatment.

[2] SEBS and other elastomers

Table 11 (to be contd.)

Properties	SEBS-18	SEBS-19	SEBS-20	SEBS-21	SEBS-22
MFR ⁽¹⁾ (g/10 min)	1.6	8	5	30	1
PS ⁽²⁾ (wt. %)	29	13	30	20	40*

Table 11 (contd.)

Properties	SEBS-23	SEBS-24	SEP	EPR
MFR ⁽¹⁾ (g/10 min)	12	0.5	0.5	0.8
PS ⁽²⁾ (wt. %)	20	20	37	-

Note: (*): Outside the range specified in the present invention.
(1) and (2) are the same as in Table 2.

[3] Talc

The same talc as in Examples 21 to 24 was used.

[4] Additives

The same additives as in Examples 1 to 10 were used except for changing the light stabilizer to Sanol LS-770 manufactured by Sankyo Company, Ltd.

The resin compositions and the test specimens were produced in the same manner as in Examples 1 to 10. The physical properties measured on each specimen are shown in Table 12.

Table 12 (to be contd.)

	Examples				
	25	26	27	28	29
Composition					
PP					
Kind	PP-9	PP-10	PP-10	PP-10	PP-10
Blend ratio (wt. %)	57	57	57	57	56
Elastomer					
Kind	SEBS-18 /SEBS-19	SEBS-18 /SEBS-19	SEBS-18 /SEBS-19 /SEBS-21	SEBS-18 /SEBS-19 /SEBS-23	SEBS-18 /SEBS-19
Blend ratio (wt. %)	17/6	11.5/11.5	11.5/6.5/5	11.5/6.5/5	12/12
Talc					
Blend ratio (wt. %)	20	20	20	20	20
Properties					
MFR ⁽¹⁾ (g/10 min)	25	31	36	37	33
Tensile strength ⁽²⁾ (kg/cm ²)	232	229	229	229	220
Elongation at break ⁽³⁾ (%)	430	600	460	600	600
Bending modulus ⁽⁴⁾ (kg/cm ²)	21900	23700	23900	23000	22000
Bending strength ⁽⁵⁾ (kg/cm ²)	353	342	343	336	334
Izod impact strength ⁽⁶⁾ (kg-cm/cm)					
at 23°C	40.0	42.0	38.3	37.1	42.1
at -30°C	4.4	6.0	4.4	4.5	5.3
Heat distortion temperature ⁽⁷⁾ (°C)	80	80	78	77	78
Rockwell hardness ⁽⁸⁾	76	74	75	73	70
Embrittle temperature ⁽⁹⁾ (°C)	-24	-25	-24	-24	-34

Table 12 (contd.)

	Examples			
	30	31	32	33
Composition				
PP				
Kind	PP-9	PP-9	PP-11	PP-10
Blend ratio (wt. %)	60	57	57	57
Elastomer				
Kind	SEBS-18 /SEBS-19	SEBS-18 /SEBS-23	SEBS-18 /SEBS-21	SEBS-18 /SEBS-20
Blend ratio (wt. %)	10/10	11.5/11.5	11.5/11.5	11.5/11.5
Talc				
Blend ratio (wt. %)	20	20	20	20
Properties				
MFR ⁽¹⁾ (g/10 min)	33	28	26	27
Tensile strength ⁽²⁾ (kg/cm ²)	257	242	241	244
Elongation at break ⁽³⁾ (%)	420	420	460	500
Bending modulus ⁽⁴⁾ (kg/cm ²)	25400	24400	24700	24900
Bending strength ⁽⁵⁾ (kg/cm ²)	393	364	355	369
Izod impact strength⁽⁶⁾ (kg-cm/cm)				
at 23°C	30.0	36.5	35.4	34.4
at -30°C	3.0	4.2	3.8	3.4
Heat distortion temperature ⁽⁷⁾ (°C)	84	80	80	79
Rockwell hardness ⁽⁸⁾	85	77	75	77
Embrittle temperature ⁽⁹⁾ (°C)	-15	-20	-18	-16

Table 12 (contd.)

	Comparative Examples		
	14	15	16
Composition			
PP			
Kind	PP-12	PP-13	PP-9
Blend ratio (wt. %)	57	57	57
Elastomer			
Kind	SEBS-18 /SEBS-22	SEP	EPR

Blend ratio (wt. %)	11.5/11.5	23	23
Talc			

Blend ratio (wt. %)	20	20	20
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Properties

MFR ⁽¹⁾ (g/10 min)	28	29	20
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Tensile strength ⁽²⁾ (kg/cm ²)	243	215	210
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Elongation at break ⁽³⁾ (%)	120	20	30
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Bending modulus ⁽⁴⁾ (kg/cm ²)	24900	23200	23600
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Bending strength ⁽⁵⁾ (kg/cm ²)	368	322	330
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Izod impact strength ⁽⁶⁾ (kg-cm/cm)			
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at 23°C	15.0	23.0	21.0
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at -30°C	3.3	5.6	3.0
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Heat distortion temperature ⁽⁷⁾ (°C)	78	77	70
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Rockwell hardness ⁽⁸⁾	80	74	65
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Embrittle temperature ⁽⁹⁾ (°C)	-3	-26	-5
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Note: (1) to (5), and (7) to (8) are the same as in Table 3, and (6) and (9) are the same as in Table 6.

As seen from the results, each resin composition of Examples 25 to 33 had an MFR showing a good fluidity and well-balanced mechanical properties. On the other hand, the comparative examples showed a poor ductility and impact strength, and had a high brittle temperature. In particular, the comparative examples where SEP or EPR was used were poor in the tensile properties and bending properties.

EXAMPLES 34 to 38 and COMPARATIVE EXAMPLES 17 to 18

The ingredients of the thermoplastic resin composition used here are shown below.

[1] Homopolypropylene (HPP)

Table 13

Properties	HPP-1	HPP-2	HPP-3	HPP-4	HPP-5	HPP-6
MFR ⁽¹⁾ (g/10 min)	20	100	160	300	600	160

$C_v^{(2)}$ (wt. %)	0	0	0	0	0	0
$G_v^{(3)}$ (wt. %)	0	0	0	0	0	0
IPF ⁽⁴⁾ (%)	97.7	97.8	97.6	97.5	98.0	97.8

Note: (1) to (3) are the same as in Table 1, and (4) is the same as in Table 4.

The MFR of each of HPP-2 to HPP-5 was regulated to the respective value by melt-extruding HPP-1 at 200°C in the presence of an organic peroxide (2,5-dimethyl-2,5-di(t-butylperoxy)hexane) to reduce the molecular weight. HPP-6 and BPP-9 were not subjected to such a treatment.

[2] SEBS and other elastomers

Table 14

Properties	SEBS-25	SEBS-26	SEPS	EPR
MFR ⁽¹⁾ (g/10 min)	1.6	8	0.5	0.8
PS ⁽²⁾ (wt. %)	29	13	13	-

Note: (1) and (2) are the same as in Table 2.

[3] Talc

The same talc as used in Examples 1 to 10 was used.

[4] Additives

The same additives as used in Examples 1 to 10 were used.

The resin compositions and the test specimens were produced in the same manner as in Examples 1 to 10. The physical properties measured on each specimen are shown in Table 15.

Table 15 (to be contd.)

	Examples			
	34	35	36	37
Composition				
First propylene polymer				
Kind	HPP-1	HPP-1	HPP-1	HPP-1
Blend ratio (wt. %)	10	20	26	33
Second propylene polymer				
Kind	HPP-3	HPP-3	HPP-4	HPP-5

	Blend ratio (wt. %)	48	38	32	25
	Elastomer				
5	Kind	SEBS-25	SEBS-25 /SEBS-26	SEBS-25 /SEBS-26	SEBS-25 /SEBS-26
	Blend ratio (wt. %)	22	11/11	11/11	11/11
	Talc				
10	Blend ratio (wt. %)	20	20	20	20
	<u>Properties</u>				
	MFR ⁽¹⁾ (g/10 min)	32	30	33	31
15	Tensile strength ⁽²⁾ (kg/cm ²)	237	236	235	235
	Elongation at break ⁽³⁾ (%)	500	500	500	500
20	Bending modulus ⁽⁴⁾ (kg/cm ²)	23500	23500	24000	23500
	Bending strength ⁽⁵⁾ (kg/cm ²)	350	350	351	350
	Izod impact strength ⁽⁶⁾ (kg-cm/cm)				
25	at 23°C	40	42	40	41
	at -30°C	4.3	4.5	4.2	4.4
	Heat distortion temperature ⁽⁷⁾ (°C)	77	78	77	77
30	Rockwell hardness ⁽⁸⁾	76	76	76	76
	Embrittle temperature ⁽⁹⁾ (°C)	-20	-22	-21	-20

Table 15 (contd.)

	<u>Example</u>	<u>Comparative Examples</u>	
	38	17	18
40	<u>Composition</u>		
	First propylene polymer		
	Kind	HPP-1	-
	Blend ratio (wt. %)	10	-
45	Second propylene polymer		
	Kind	HPP-6	HPP-2
	Blend ratio (wt. %)	48	58
50	Elastomer		
	Kind	SEBS-25	SEPS
	Blend ratio (wt. %)	22	22
55	Talc		
	Blend ratio (wt. %)	20	20

Properties

MFR ⁽¹⁾ (g/10 min)	35	24	25
Tensile strength ⁽²⁾ (kg/cm ²)	240	225	225
Elongation at break ⁽³⁾ (%)	500	50	60
Bending modulus ⁽⁴⁾ (kg/cm ²)	23500	23000	23800
Bending strength ⁽⁵⁾ (kg/cm ²)	350	350	340
Izod impact strength ⁽⁶⁾ (kg-cm/cm)			
at 23°C	40	10	12
at -30°C	4.2	3.0	2.5
Heat distortion temperature ⁽⁷⁾ (°C)	76	72	73
Rockwell hardness ⁽⁸⁾	76	73	70
Embrittle temperature ⁽⁹⁾ (°C)	-18	-6	0

Note: (1) to (9) are the same as in Table 6.

As seen from the results, each resin composition of Examples 34 to 38 had an MFR showing a good fluidity and well-balanced mechanical properties. The comparative example containing SEPS or EPR was insufficient in ductility and impact strength, and had a high brittle temperature.

EXAMPLES 39 to 45 and COMPARATIVE EXAMPLES 19 to 20

The ingredients of the thermoplastic resin composition used here are shown below.

[1] Homopolypropylene (HPP) and Ethylene-propylene random copolymer (RPP)

Table 16 (to be contd.)

Properties	HPP-7	HPP-8	HPP-9	HPP-10
MFR ⁽¹⁾ (g/10 min)	2	20	160	200
IPF ⁽²⁾ (%)	94.9	94.8	97.5	97.8
C _v ⁽³⁾ (wt. %)	0	0	0	0
C ₂ ⁽⁴⁾ (wt. %)	0	0	0	0

Table 16 (contd.)

Properties	HPP-11	HPP-12	RPP-1	RPP-2
MFR ⁽¹⁾ (g/10 min)	300	160	3	5
IPF ⁽²⁾ (%)	97.5	98.0	-	-
C _V ⁽³⁾ (wt. %)	0	0	-	-
C ₂ ⁽⁴⁾ (wt. %)	0	0	0.4	0.6

Note: (1) and (3) are the same as in Table 1, and (2) is the same as in Table 4.

(4): C₂ is the ethylene content in the propylene polymer.

The MFR of each of HPP-4 to HPP-7 was regulated to the respective value by melt-extruding HPP-3 at 200°C in the presence of an organic peroxide (2,5-dimethyl-2,5-di(t-butylperoxy)hexane) to reduce the molecular weight. The other propylene polymers were not subjected to such a treatment.

[2] SEBS and other elastomers

Table 17

Properties	SEBS-27	SEBS-28	SEPS	EPR
MFR ⁽¹⁾ (g/10 min)	1.6	8	0.5	0.8
PS ⁽²⁾ (wt. %)	29	13	13	-

Note: (1) and (2) are the same as in Table 2.

[3] Talc

The same talc as used in Examples 1 to 10 was used.

[4] Additives

The same additives as used in Examples 1 to 10 were used.

The resin compositions and the test specimens were produced in the same manner as in Examples 1 to 10. The physical properties measured on each specimen are shown in Table 18.

Table 18 (to be contd.)

Composition	Examples				
	39	40	41	42	43
First propylene polymer					

	Kind	RPP-1	RPP-2	HPP-7	HPP-8	HPP-8
	Blend ratio (wt. %)	10	10	10	10	20
5	Second propylene polymer					
	Kind	HPP-10	HPP-10	HPP-10	HPP-9	HPP-9
	Blend ratio (wt. %)	48	48	48	48	38
10	Elastomer					
	Kind	SEBS-27 /SEBS-28	SEBS-27 /SEBS-28	SEBS-27 /SEBS-28	SEBS-27	SEBS-27 /SEBS-28
	Blend ratio (wt. %)	11/11	11/11	11/11	22	11/11
15	Talc					
	Blend ratio (wt. %)	20	20	20	20	20
	Properties					
20	MFR ⁽¹⁾ (g/10 min)	31	32	30	32	30
	Tensile strength ⁽²⁾ (kg/cm ²)	240	238	239	237	236
	Elongation at break ⁽³⁾ (%)	600	600	600	600	600
25	Bending modulus ⁽⁴⁾ (kg/cm ²)	23500	23400	23600	23500	23500
	Bending strength ⁽⁵⁾ (kg/cm ²)	352	350	351	350	350
30	Izod impact strength ⁽⁶⁾ (kg-cm/cm)					
	at 23°C	42	43	42	40	42
	at -30°C	4.4	4.5	4.3	4.3	4.5
35	Heat distortion temperature ⁽⁷⁾ (°C)	76	76	77	77	78
	Rockwell hardness ⁽⁸⁾	76	76	76	76	76
40	Embrittle temperature ⁽⁹⁾ (°C)	-20	-22	-21	-20	-22

Table 18 (contd.)

45		<u>Examples</u>		<u>Comparative Examples</u>	
		44	45	19	20
	Composition				
	First propylene polymer				
50	Kind	HPP-8	HPP-8	RPP-1	RPP-1
	Blend ratio (wt. %)	26	10	57	57
	Second propylene polymer				
55	Kind	HPP-11	HPP-12	-	-
	Blend ratio (wt. %)	32	48	-	-

Elastomer				
Kind	SEBS-27 /SEBS-28	SEBS-27	SEPS	EPR
Blend ratio (wt. %)	11/11	22	23	23
Talc				
Blend ratio (wt. %)	20	20	20	20
<u>Properties</u>				
MFR ⁽¹⁾ (g/10 min)	33	35	33	35
Tensile strength ⁽²⁾ (kg/cm ²)	235	236	220	220
Elongation at break ⁽³⁾ (%)	600	600	30	40
Bending modulus ⁽⁴⁾ (kg/cm ²)	24000	23500	23100	23300
Bending strength ⁽⁵⁾ (kg/cm ²)	351	350	344	335
Izod impact strength ⁽⁶⁾ (kg-cm/cm) at 23°C	40	40	10	12
at -30°C	4.2	4.5	3.0	2.4
Heat distortion temperature ⁽⁷⁾ (°C)	77	77	72	73
Rockwell hardness ⁽⁸⁾	76	76	73	71
Embrittle temperature ⁽⁹⁾ (°C)	-21	-20	-3	-1

Note: (1) to (9) are the same as in Table 6.

As seen from the results, each resin composition of Examples 39 to 45 had an MFR showing a good fluidity and well-balanced mechanical properties. The comparative example containing SEPS or EPR was insufficient in ductility and impact strength, and had a high brittle temperature.

As described above, the thermoplastic resin composition of the present invention is excellent in the moldability and the ductility, and can provide a molded article having mechanical properties well balanced. Therefore, with such a resin composition, the injection molding conditions can be widely selected, and a large-sized article with a thin wall can be easily molded. The resin composition of the present invention is suitable for injection molding, for example, a inner or outer lining material for automobiles and an appliance part.

Claims

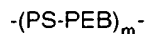
1. A thermoplastic resin comprising:

(A) 30 to 80 weight % of a propylene polymer component;

(B) a styrene-containing elastomer component selected from the groups consisting of:

(a) 10 to 30 weight % of an elastomeric styrene-containing block copolymer having a melt flow rate of 0.5 to 40 g/10 min and a polystyrene block content of 10 to 30 weight % and being represented by formulae (I) or (II):





(II)

wherein PS is said polystyrene block, PEB is a poly(ethylene-butene) block and m is an integer of 1 or more; and

(b) 5 to 30 weight % of a binary elastomer, comprising:

- (i) 40 to 80 weight % of at least one elastomeric styrene-containing block copolymer having a melt flow rate of 0.5 to 3 g/10 min and a polystyrene block content of 10 to 30 weight %; and
- (ii) 20 to 60 weight % of at least one other elastomeric styrene-containing block copolymer having a melt flow rate of 4 to 100 g/10 min and a polystyrene block content of 10 to 30 weight %;

wherein each of said elastomeric styrene-containing block copolymers are represented by formulae (I) or (II); and

(C) 10 to 40 weight % of talc having an average particle size of 5 μm or less.

2. The thermoplastic resin composition according to claim 1, wherein said propylene polymer component is an ethylene-propylene block copolymer having a melt flow rate of 30 to 200 g/10 min and comprising (a) 70 to 99 weight % of a crystalline propylene polymer block and (b) 1 to 30 weight % of an ethylene-propylene copolymer block having an ethylene content of 20 to 80 weight % and an intrinsic viscosity $[\eta]_{\text{CXS}}$ of 2 to 7 dl/g.

3. The thermoplastic resin composition according to claim 1, wherein said propylene polymer component is a polypropylene resin having a melt flow rate of 20 to 200 g/10 min, an isotactic pentad fraction of 95 % or more and a copolymer block content of 0 to 2 weight %.

4. The thermoplastic resin composition according to any one of claims 1 to 3, wherein a difference in the melt flow rate between said elastomeric styrene-containing block copolymer having a melt flow rate of 4 to 100 g/10 min and said elastomeric styrene-containing block copolymer having a melt flow rate of 0.5 to 3 g/10 min, each constituting said binary elastomer, is 3 g/10 min or more.

5. The thermoplastic resin composition according to claim 1, wherein said propylene polymer component comprises:

10 to 50 weight %, based on the total of the essential components, of at least one first propylene polymer component selected from the group consisting of a first homopolypropylene and a first ethylene-propylene block copolymer, each having a melt flow rate of 2 to 30 g/10 min; and

10 to 50 weight %, based on the total of the essential components, of at least one second propylene polymer component selected from the group consisting of a second homopolypropylene and a second ethylene-propylene block copolymer, each having a melt flow rate of 50 to 1000 g/10 min;

and wherein said styrene-containing elastomer component is the elastomeric styrene-containing block copolymer (a).

6. The thermoplastic resin composition according to claim 1, wherein said propylene polymer component comprises:

10 to 50 weight %, based on the total of the essential components; of at least one first propylene polymer component selected from the group consisting of a first homopolypropylene and an ethylene-propylene random copolymer, said first homopolypropylene having a melt flow rate of 2 to 30 g/10 min and an isotactic pentad fraction of 90 to 95%, and said ethylene-propylene random copolymer having a melt flow rate of 2 to 30 g/10 min and an ethylene content of 0.1 to 1 weight %; and

10 to 50 weight %, based on the total of the essential components, of a second homopolypropylene having a melt flow rate of 50 to 1000 g/10 min;

and wherein said styrene-containing elastomer component is the elastomeric styrene-containing block copolymer (a).

7. The thermoplastic resin composition according to claim 5 or 6, wherein the melt flow rate of said second homopol-

propylene is regulated within the range of 50 to 1000 g/10 min by subjecting a homopolypropylene having a melt flow rate smaller than 50 g/10 min to a chain length regulating treatment.

8. A process for producing a thermoplastic resin composition as claimed in claim 1 or 2 which comprises blending components (A), (B) and (C) as claimed in claim 1 or 2 and optionally extruding the mixture to produce pellets of said thermoplastic resin composition.
9. An article prepared from a thermoplastic resin composition as claimed in claims 1 to 7.



European Patent
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EUROPEAN SEARCH REPORT

Application Number
EP 97 30 1412

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
X	EP 0 463 963 A (NISSAN MOTOR ;UBE INDUSTRIES (JP)) 2 January 1992	1-3	C08L23/10
Y	* claims *	5,6	C08L53/00
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X	US 5 283 267 A (NISHIO TAKEYOSHI ET AL) 1 February 1994	1-3	
Y	* claims *	5,6	

X	EP 0 697 435 A (TOYOTA MOTOR CO LTD ;UBE INDUSTRIES (JP)) 21 February 1996	1-4	
Y	* claims *	5,6	

X	GB 2 281 302 A (UBE INDUSTRIES, LTD.) 1 March 1995	1-3	
Y	* claims *	5,6	

Y	US 5 045 589 A (UENO KOUHEI) 3 September 1991	5,6	
	* column 3, line 28 - line 33; claims *		

			TECHNICAL FIELDS SEARCHED (Int.Cl.6)
			C08L
The present search report has been drawn up for all claims			
Place of search		Date of completion of the search	Examiner
THE HAGUE		23 June 1997	Clemente Garcia, R
CATEGORY OF CITED DOCUMENTS			
<p>X : particularly relevant if taken alone</p> <p>Y : particularly relevant if combined with another document of the same category</p> <p>A : technological background</p> <p>O : non-written disclosure</p> <p>P : intermediate document</p> <p>T : theory or principle underlying the invention</p> <p>E : earlier patent document, but published on, or after the filing date</p> <p>D : document cited in the application</p> <p>L : document cited for other reasons</p> <p>& : member of the same patent family, corresponding document</p>			

EPO FORM 150 03.82 (P04C01)

1. The first part of the document is a letter from the President of the United States to the Congress, dated January 3, 1862. It is a very important document, as it contains the President's annual message to Congress. The letter is written in a very formal and dignified style, and it is one of the most important documents in the history of the United States.

2. The second part of the document is a report from the Secretary of the Interior, dated January 3, 1862. It is a very important document, as it contains the Secretary's annual report to the President. The report is written in a very formal and dignified style, and it is one of the most important documents in the history of the United States.

3. The third part of the document is a report from the Secretary of the Treasury, dated January 3, 1862. It is a very important document, as it contains the Secretary's annual report to the President. The report is written in a very formal and dignified style, and it is one of the most important documents in the history of the United States.

4. The fourth part of the document is a report from the Secretary of the War, dated January 3, 1862. It is a very important document, as it contains the Secretary's annual report to the President. The report is written in a very formal and dignified style, and it is one of the most important documents in the history of the United States.

5. The fifth part of the document is a report from the Secretary of the Navy, dated January 3, 1862. It is a very important document, as it contains the Secretary's annual report to the President. The report is written in a very formal and dignified style, and it is one of the most important documents in the history of the United States.

6. The sixth part of the document is a report from the Secretary of the State, dated January 3, 1862. It is a very important document, as it contains the Secretary's annual report to the President. The report is written in a very formal and dignified style, and it is one of the most important documents in the history of the United States.

7. The seventh part of the document is a report from the Secretary of the War, dated January 3, 1862. It is a very important document, as it contains the Secretary's annual report to the President. The report is written in a very formal and dignified style, and it is one of the most important documents in the history of the United States.

8. The eighth part of the document is a report from the Secretary of the Navy, dated January 3, 1862. It is a very important document, as it contains the Secretary's annual report to the President. The report is written in a very formal and dignified style, and it is one of the most important documents in the history of the United States.

9. The ninth part of the document is a report from the Secretary of the State, dated January 3, 1862. It is a very important document, as it contains the Secretary's annual report to the President. The report is written in a very formal and dignified style, and it is one of the most important documents in the history of the United States.

10. The tenth part of the document is a report from the Secretary of the War, dated January 3, 1862. It is a very important document, as it contains the Secretary's annual report to the President. The report is written in a very formal and dignified style, and it is one of the most important documents in the history of the United States.